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NIOSH HEALTH HAZARD EVALUATION REPORT

NIOSH

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Introduction

In February 2003, the National Institute for Occupational Safety and Health (NIOSH) received a request for a Health Hazard Evaluation (HHE) from the vice-president of the Genesis Steel Service, Inc (GSSI). GSSI, a construction reinforcing and structural steel contractor in Baltimore, MD, GSSI asked NIOSH to do the following:

- Evaluate the risk that GSSI reinforcing ironworkers have for developing back and hand musculoskeletal disorders as a result of hand-tying reinforcement steel on concrete bridge decks, and
- Investigate whether the use of a battery powered tier (BPT) for rebar tying can be an effective intervention for the prevention of work-related musculoskeletal disorders (WMSDs) of the upper extremities and back.

In response to the request, NIOSH investigators conducted a field investigation of GSSI employees' exposures to biomechanical loading when tying rebar for the concrete deck of an elevated freeway bridge in Springfield, VA. The investigation was conducted on October 27-30, 2003.

Background

Genesis Steel Service, Inc. is a minority owned construction specialty subcontractor providing structural and reinforcing steel services for new construction projects in the greater Baltimore-District of Columbia metropolitan area. The distribution of GSSI's work is approximately 60% concrete reinforcement, 25% structural (bridge and buildings < 4 stories), and 15% miscellaneous metals, including ornamental. GSSI does not operate a fabrication shop and reinforcing steel used on projects is predominantly pre-cut and pre-formed.

At the time of the HHE request, GSSI employed 100 ironworkers (IWs). Around 40% of the IWs employed by GSSI were minority workers - 20% African-American and 20% Hispanic. GSSI estimated that for 2/3 of the Hispanic workers English is their second language. The IWs are members of the International Association of Bridge, Ornamental, and Reinforcing Iron Workers. GSSI estimated that 25-30% of the IWs employed at the time of the study had been employed by the contractor since 1988. Genesis' IWs tend to specialize in structural or reinforcing work, and most reinforcing ironworkers (RIW), also known as 'rodmen', work exclusively on concrete reinforcing jobs.

Springfield Interchange Freeway Bridge

As a subcontractor on the Springfield Interchange Improvement Project, GSSI installed reinforcing steel bars for the concrete deck of the bridge connecting westbound I-495 traffic to the southbound I-95 interstate highway. The bridge is approximately one mile long by 60 feet wide. GSSI employees were responsible for placing and tying the steel bars used to reinforce the concrete deck and walls of the bridge. An estimated 2.2 million wire ties were made on the bridge to secure the rebar at a rate of 7 wire ties per square foot (ft²) for the bridge. For most of the project, weather permitting, GSSI IWs worked a 5 day and 40 hour work week. The amount of rebar placed and tied on a given day depended on several factors, including the number of workers on the job, the environmental conditions, and the pace of the work preceding rebar installation.

Installing and Fastening Rebar for the Bridge

Before pouring the concrete deck that will be the surface of the bridge, steel reinforcing bars (aka rebar) must be placed inside the concrete forms. The rebar is used to reinforce and increase the tensile strength (i.e., bending and stretching) of the concrete in the deck and sidewalls. Two

rebar ‘mats’ were placed one above the other inside the concrete form over the full length of the bridge. Each mat consisted of a series of bars placed perpendicular to each other and spaced about seven (7) inches on-center. The bottom mat was kept above the metal decking using wire supports (aka chairs). Chairs were used to separate the top mat from the bottom mat. The rebar are tied together to prevent the bars from shifting when the concrete mixture is poured into the form, although the ties do not add strength to the bridge.

The specifications for the job, common for freeway bridge decks in the United States, required tying 50% of the intersecting rebar on the bottom mat and 100% of the intersections on the top mat. GSSI employees used two techniques to tie the intersecting rebar together, including: 1) pliers and spool of wire and 2) the battery operated RB392 rebar tier (MAX USA Corp., Garden City, New York) (Figure 1). The BPT tier was used most frequently to make the ‘snap’ or simple ties used to keep the rebar from shifting. Pliers were used when more secure ties (i.e., ‘saddle’ or ‘figure 8’) were necessary to frame the sidewalls of the bridge deck or make the first ties for each mat (Figure 2).

Traditional tying (Figure 3) required the use of two hands – one to use the pliers to pull, wrap, twist, and cut the wire and the other to pull and push the wire. Only one hand was necessary to operate the BPT (Figure 4). Both techniques required frequent and sustained deep trunk bending (aka stooping) (>90° trunk inclination) to tie the rebar.

NIOSH introduced a commercially available extension handle developed for use with the BPT (Figure 5 and 6). This was the third rebar tying technique used during the investigation.

Methods

GSSI employees were directed to tie the rebar placed for the bottom mat using three different tying techniques: 1) pliers; 2) the RB392 BPT

and 3) the BPT with an extension handle (BPT+E). All employees were familiar with the first two techniques and used each on the site. NIOSH brought the extension handle to the site and none of the employees had previously used

the device. Participants were encouraged, but not required, to use the extension before measurements were made.

GSSI had purchased the BPTs approximately 2 years prior to the study in part to reduce employees’ exposures to biomechanical loading related to tying using pliers. The power tier still required deep forward bending when tying at deck level, but workers now used one hand to hold the tier and the other to support their upper body while tying.

The investigation was conducted to answer the following questions:

1. How does the use of a battery powered rebar tier (MAX USA RB392) affect the biomechanical loading of the hand-wrist and/or of the low back?
2. How does the use of an adjustable extension handle with the battery powered rebar tier (MAX USA RB392) affect the biomechanical loading of the hand-wrist and/or low back?
3. How does the use of the battery powered rebar tier (MAX USA RB392) with and without the adjustable handle affect the productivity of rebar tying?

Data collection

Each worker tied rebar for about 30 minutes using the: 1) pliers; 2) BPT; and 3) BPT+E. A twin-axis goniometer (Biometrics SG Series) and torsionmeter (Biometrics Q110) were used to measure the dominant wrist motion and position (aka posture) in the flexion/extension, ulnar/radial, and pronation/supination planes (Figure 7) during tying.¹ Observational methods were used to record the position of the trunk during tying and the number of ties each worker made. This consisted

of videotaping each worker from three different angles so that the trunk could be later viewed from both the side and front.

Each worker was asked to describe the physical effort they used with their hand-wrist and lowback on a scale from 0 ('nothing at all') to 10 ('extremely strong') when using the three tying methods.² Prior to conducting the study, the 10-point scale was translated into Spanish by a NIOSH contractor.

Personal information and work history was obtained using self administered questionnaires available in English and Spanish.

Data Analyses

Goniometric data

The goniometric data were converted to readable files using proprietary Biometrics Ltd. management and analysis software. Statistical analysis, including summary and inferential statistics, was conducted using SAS® Institute software.

Positional data

Video tape was analyzed using the Multimedia Video Task Analysis (MVTATM) software program, which allowed the analyst to run video tape through the computer.³ The analyst recorded the frequency and duration of the trunk posture angles and the time required to tie rebar for each of the three tying techniques.

Analysts used the computer-based 3-D Static Strength Prediction Program™ to estimate the pressure (compressive forces) on the spinal disc between the fifth lumbar vertebrae and the first sacral vertebrae (aka L5/S1 spinal disc) during rebar tying in stooped postures.⁴ Disc pressure is known to vary depending on the amount and type (e.g., forward, sideward, twisting) of bending.

Evaluation criteria

Overexertion injuries and musculoskeletal disorders, such as low back pain, tendinitis, and carpal tunnel syndrome, are often associated with job tasks that include:

1. Repetitive, stereotyped movement about the joints;
2. Forceful manual exertions;
3. Lifting, pushing, and pulling;
4. Awkward and/or static body positions;
5. Direct pressure on nerves and soft tissues;
6. Work in cold environments;
7. Exposure to whole-body or segmental vibration; or
8. Work-related psychosocial factors, such as high job demand, low decision latitude, and monotonous activity, etc.

The risk of injury appears to increase as the intensity and duration of exposures to the risk factors increases and the recovery time (i.e., rest time) decreases. Individual characteristics (e.g., age, gender, weight, fitness) are seen as "contributing and modifying influences in the development of pain and disability and in the transition from acute to chronic pain."⁵

The preferred method for preventing and controlling work-related musculoskeletal disorders (WMSDs) is to reduce or eliminate exposure to the risk factors. The most effective way to do this is to design jobs, workstations, tools, and other equipment to match the physiological, anatomical, and psychological characteristics and capabilities of the worker. Under these conditions, exposures to task factors considered potentially hazardous will be reduced or eliminated.

The following criteria were used to evaluate the biomechanical loading of GSSI employees' low back and upper limbs during rebar tying tasks on the Springfield Interchange Improvement Project:

1. the American Conference of Governmental Industrial Hygienists (ACGIH™) Hand Activity Level (HAL) Threshold Limit Value (TLV)™,⁶
2. recommendations for acceptable hand-wrist motion (e.g., velocity and acceleration) to prevent wrist cumulative trauma disorders (CTD),^{7,8}
3. the Michigan 3-Dimensional Static Strength Prediction Program™ to estimate the compressive and shear forces on the L5/S1 spinal disc,⁴
4. the Evaluation of Static Working Postures, International Organization for Standardization (ISO) 11226,⁹ and
5. risk assessment of spinal disease as a result of cumulative physical work load on the lumbar spine.¹⁰

ACGIH™ Hand Activity Level TLV™

The ACGIH™ Hand Activity Level (HAL) TLV™ is based on epidemiological, psychophysical, and biomechanical studies and is applied to "mono-task" jobs performed for four hours or more per day. (A mono-task job involves performing a similar set of motions or exertions repeatedly such as working on an assembly line or using a keyboard for transcription.) The HAL is based on the frequency of hand exertions and the duty cycle (distribution of work and recovery periods). The HAL can be determined by a trained observer or calculated using information on the frequency of exertions and the work/recovery ratio. Peak force is normalized on a scale of 0 to 10, corresponding to 0% to 100% of the applicable population reference strength. Peak force can be determined with ratings by a trained observer, ratings using subjective exertion scales (i.e., Borg 10 point perceived effort scale)², or measured using instrumentation such as strain gauges. Peak force requirements can be normalized by dividing the force required to perform the job by the strength capability of the work population for that activity. The total exposure is characterized in terms of average hand activity level and peak hand force.

Hand-Wrist Motion Guidelines

Marras and Schoenmarklin studied the relationship between wrist movement, including the angle, repetition, velocity, and acceleration levels, and the risk of developing a CTD.⁷ The study found that high wrist and forearm motion (i.e., angular velocity and angular acceleration) during an 8-hour day were significantly associated with risk of developing an upper extremity CTD. Non-neutral wrist position (aka posture) alone was not associated with an increased risk of developing CTDs. Mean wrist acceleration levels associated with high and low CTD risk in the radial/ulnar, flexion/extension, and pronation/supination planes were, respectively, 494 and 301 angular degrees/second² (d/s²), 824 and 494 d/s², and 1824 and 1222 d/s². In follow-up analysis of the data, wrist acceleration in the flexion/extension plane was determined to be the best predictor of a hand/wrist CTD.⁸

3-D Static Strength Prediction Program

The Michigan 3-Dimensional Static Strength Prediction Program™ (3DSSPP™) is a computerized model which can be used to evaluate the physical demands of a prescribed job.⁴ Typical inputs to the model are the magnitude and direction of forces at the hands, angles of body segments, and worker characteristics. The model calculates forces (i.e., moments) on the joints of the body and estimates the percentage of the work-force able to sustain the inputted loads. Compressive and shear forces for the L5/S1 disc are calculated. The program allows the analyst to estimate the compressive forces acting on the spine relative to the revised NIOSH lifting equation.¹¹ In order to prevent low back disorders, NIOSH recommends L5/S1 disc compression force never exceed 3400 Newtons (N) during any single job activity (1 N = 0.225 pound-force).

The 3DSSPP™ can be used to evaluate the biomechanical demands of an existing task or to predict the physical demands of a task that is being designed or modified. The joint angles for the

program's mannequin were set to represent postures used during rebar tying and estimate the forces exerted on the L5/S1 spinal disc.

ISO Evaluation of Static Work Postures

The ISO developed the consensus standard titled Ergonomics – Evaluation of Static Working Postures (ISO 11226-2000).⁹ ISO 11226 was written to control pain, fatigue and disorders of the musculoskeletal system that may result from the use of non-neutral body postures for long durations without sufficient recovery time. The standard describes acceptable trunk postures and maximum acceptable holding times for potentially harmful postures.

Cumulative spinal loading and back disease

Seidler et al investigated the relationship between the cumulative (e.g., added over time) forces on the lumbar section of the back and symptomatic spinal disease, e.g., spondylosis of the lumbar spine.¹² Specifically, the study compared the stress (i.e., forces) over time on the lumbar spine due to lifting, carrying, and extreme forward flexion (>90°) with the occurrence of back disease (i.e., osteochondrosis or spondylosis) diagnosed using x-rays. The authors reported significantly more spinal disease in the group of workers with the higher cumulative physical stress on the back compared with workers with less back stress. The risk of back disease also increased with the amount of physical force applied to the L5/S1 spinal disc.

Results Summary

Manually tying rebar at ground level using pliers and wire involved sustained deep trunk bending and rapid and repetitive hand and wrist movements. Using a BPT significantly reduced the use of rapid and repetitive hand-wrist and forearm movements characteristic of tying with the pliers, and freed one hand to support the weight of the trunk during tying. Adding an extension handle to the BPT allowed workers to

tie rebar standing erect. The results show that manually tying rebar using a pliers involves greater risk of developing a low back WMSD than tying with either the BPT or BPT+E. The study indicates that tying with the BPT+E also involves less risk of developing an upper limb WMSD.

Demographics

All eight GSSI employees (six Hispanic, two Caucasian) installing rebar on the freeway bridge agreed to participate in the study. Participant mean age was 37 years old and mean height, weight and body mass index (BMI) were, respectively 69 inches, 184 lbs., and 27.4 BMI (Table 1). Table 2 shows participants' mean time working as a rodbuster, employed by GSSI, and working on the study job site. Participants reported tying rebar using a pliers and using a BPT 8.1 hours/week and 6.1 hours/week, respectively. One worker reported a back injury occurring during the previous 12 months that affected his work. No injuries occurring during the previous 12 months were reported by the remaining seven workers. Electro-goniometric analyses

Calibration

The calibration results for the electrogoniometers demonstrated that the wrist position measurements were accurate and consistent.

Wrist and Forearm Movements

Wrist mean velocity and mean acceleration were higher during pliers tying than BPT or BPT+E tying. Differences between the pliers and the BPT or BPT+E rates were significantly different (Tables 3 and 4). Mean wrist velocities measured in the flexion/extension and ulnar/radial planes during pliers tying exceeded velocities associated with high and low risks of developing a CTD (Figure 8).⁷ The low CTD risk level was exceeded in the ulnar/radial plane using each of the three tying techniques. Operating the BPT resulted in a mean wrist velocity in one plane (ulnar/radial) exceeding the level associated with a high CTD risk.

Figure 9 shows that workers' mean wrist acceleration levels measured during pliers tying exceeded levels found to be associated with (a) high CTD risk in the flexion/extension (i.e., 824 d/s²) and ulnar/radial (i.e., 494 d/s²) planes and (b) low CTD risk in the pronation/supination plane (i.e., 1222 d/s²). Use of the BPT exceeded acceleration levels related to low CTD risk level in the ulnar/radial plane (i.e., 301 d/s²).⁷

Borg Perceived Effort

Five workers completed the perceived effort questionnaire. Participants reported the lowest 'low back' effort when using the BPT+E (1.2 on the 10 point Borg scale), followed by 2.8 for the BPT and 5.8 for the pliers. The lowest handwrist effort was reported for the BPT (2.8) and the BPT+E and pliers were, respectively, 5.0 and 5.2. (Table 5)

Observational analyses ACGIH Hand Activity Level TLV™

ACGIH HAL-TLV™ scores were calculated using the workers' perceived effort scores² (i.e., mean, low and high) for each tying technique. Using the mean scores, the HAL-TLV™ (0.78) would be greatly exceeded at 2.5 when a pliers was used and slightly exceeded at 0.83 when an BPT+E (0.83) was used for 4 hours or more each day. Use of the BPT alone would not exceed the HAL-TLV™. (Table 6)

Trunk Positions

Workers were observed tying rebar with severe trunk bending ($\geq 90^\circ$) 94% of the time when using the pliers and 93% of the time when using the BPT (Table 7). With the BPT+E workers tied rebar using neutral trunk positions ($< 15^\circ$ flexion) 83% of the time and moderate forward flexion ($16^\circ - 30^\circ$) 16% of the tying time with the extension attached to the power tier.

ISO 11226 recommends that working trunk postures not exceed 60° of forward bending at any time. Observed trunk postures used during pliers and BPT rebar tying greatly exceeded the

ISO 11226 recommendations.

When using the BPT, all workers used their free hand to support the weight of their torso, e.g., resting the hand/forearm on the knee/thigh, 90% of the time when they tied at ground level. (Table 8) [Note: Workers use two hands to tie using the pliers, while only one hand is necessary using the BPT or BPT+E.]

Other Cumulative trunk loading

Using the 3D Static Strength Prediction Program™ (3DSSPP)⁴, compressive and shear forces acting on the L5/S1 disc were estimated to be between 1500 N to 2850 N during two-hand rebar tying using the pliers without lateral bending or trunk rotation. (Table 9) Lateral bending (25° left or right) increased both total and shear compression forces when the trunk inclination did not change. Highest shear forces were 501 N and were recorded at the deepest trunk inclination (-125°) and 25° lateral bending. Although these forces do not exceed the NIOSH revised lifting guideline (3400 N), the postures must be sustained for several hours each day increasing the cumulative force over many years of activity.

Cumulative forces on the L5/S1 were calculated (Figure 10/Table 10) for rebar tying (average 2 and 4 hours duration/day) and carrying 20 kg (average 1 hour/day) in front of or beside the body for one, five, and ten years.¹² Figure 11 shows that the estimated cumulative forces resulted in 2.6 (95% CI 1.2 – 5.7) and 6.0 (95% CI 2.7 – 13.4) times greater risk (odds ratios) of developing spinal disease, respectively, after 5 years and 10 years work-exposure.¹²

With the trunk fully flexed, e.g., tying rebar at ground level, the muscles that normally support the spinal column become ineffective and the ligaments take over.¹³ When the lumbar spine becomes stretched out there is a greater potential for damage to the spinal discs.^{13,14}

Discussion

Risks Associated with Pliers Tying

Both the ACGIH™ HAL-TLV™ and the CTD risk estimates developed by Marras and Schoenmarklin⁸ assume exposure occurs, respectively, for ≥ 4 hours and 8 hours each day. Reinforcing ironworkers (RIWs) reported tying rebar for about 16 hours per week using the pliers or BPT. Tying rebar using the pliers for 4 or more hours each day exceeded the ACGIH™ HAL-TLV™ by 3.2 times. Using the BPT+E for 4 hours or more each day slightly exceeds the HAL-TLV™.

During pliers tying, wrist motion (i.e., mean velocity and acceleration) in the flexion/extension and ulnar/radial planes was about twice as fast as the motion associated with both low and high CTD risk reported by Marras and Schoenmarklin.⁷ The upper limb CTD risk assessment they conducted was for an 8-hours work day. RIWs who do not continuously tie rebar with a pliers for 8 hours may not exceed these parameters.

However, pliers tying requires rapid wrist movement in all three planes of motion in combination with hand forces necessary to pull, twist, and cut the wire. Marras and Schoenmarklin⁷ did not describe the combined effect of rapid motion in multiple planes and, therefore, the CTD risk levels reported may underestimate actual risk when rapid motions are required in all three planes.

The frequency and duration of extreme trunk flexion using the pliers increases RIWs' exposure to risk factors for lumbar spine disease after 5-10 years of tying in a stooped posture and put them at greater risk of developing a low back disorder.

The results of the study clearly show that manually tying rebar using a pliers exposes workers to serious risk factors for developing WMSDs of low back and the upper limbs.

Tying Using the BPT and BPT+E Hand-Wrist

Use of the BPT resulted in mean hand-activity level scores below the ACGIH HAL-TLV™. The BPT+E resulted in a mean hand-activity level slightly higher than the TLV™. This difference can be explained by the higher “perceived effort” scores RIWs gave the BPT+E on the Borg2 questionnaire. Unlike the BPT, workers did not have experience using the extension prior to the study. Use of the extension does increase the distance of the hand to the tying location, and possibly reduces control of the tool during placement. Perhaps more importantly, however, positioning and holding the BPT+E away from the body results in higher forces on the hand, arm, and shoulder due to the larger moment. These factors likely increased the “perceived effort” scores during BPT+E use and could be addressed with training.

There was no significant difference between the wrist movement (i.e., velocity and acceleration) when comparing the use of the BPT and BPT+E. Vi described an increase in productivity for the BPT+E comparable to the BPT in a study of union RIWs in Ontario, Canada, who had experience using the extension before the study began.¹⁵

Low Back

Use of the BPT+E resulted in the least forward bending during rebar tying. Although the BPT tying trunk positions were not significantly different from pliers tying positions, it is reasonable to assume there is less loading on the lumbar spine. The BPT only requires the use of one hand to tie rebar and all workers were observed using the free hand to support their upper body weight during the majority of the time they were observed tying with the BPT. The use of the hand or arm to support the upper body should reduce the compressive forces applied to the lumbar spine. Participants appear

to have confirmed this when they reported significantly less perceived effort for the low back using the BPT+E than the pliers (2.8 for the BPT+E and 5.8 for the pliers), despite the similar posture.

Other Activities

NIOSH analyzed only rebar tying during this study, although reinforcing ironworkers' perform additional job activities that require "maximum muscle force to lift, push, pull, or carry objects."¹⁶ For example, in addition to lifting and carrying rebar, workers must also separate individual rebar from the bundles transported to the immediate work area. Rebar transported in bundles can become intertwined, which makes the separation of individual rebar lengths difficult. Workers were observed separating rebar using sudden (i.e., jerking) muscle forces – often in stooped and asymmetrical postures- to separate individual rebar from the bundles.

RIWs' manual material handling activities can comprise a significant percentage of work time. Forde¹⁷ reported "(m)anual material handling (MMH) activities (lifting, lowering, pushing, pulling, dragging, carrying, holding, forceful motions) were observed 22% and 32% of the observed time", respectively, for reinforcing ironworkers building caisson cages and the deck and sides of a freeway access tunnel. If these additional activities had been evaluated during the study, the estimates would be higher and indicate greater risk of developing a back musculoskeletal disorder.

Study Limitations

There are three limitations of this study. First, participants' time using the extension handle (BPT+E) was measured in minutes, rather than hours. Subsequently, most, if not all, participants had insufficient time to become accustomed to using the extension (BPT+E). The wrist, elbow, and shoulder can be subjected to larger moments

when the tool is positioned and held further from the body. This unfamiliarity may explain some participants higher hand-wrist perceived effort ratings.

Second, the study was not conducted in a manner that could determine the real productivity differences among the three tying techniques. Using the BPT nearly doubled the number of ties completed during the analysis periods, while the BPT+E resulted in a slight increase. The observation time, however, was too short to consider possible non-productive time related to using the BPT, such as the additional cost of charging BPT batteries (using gasoline powered generator) on the construction site and potential productivity loss due to changing batteries and BPT mechanical failure, i.e., wire jam. Despite this shortcoming, GSSI ironworkers and management representatives expressed confidence that the MAX USA RB392 power tier increased workers' productivity.

Conclusions

1. Manually tying rebar using a pliers exceeded the ACGIH™ HAL-TLV™ and wrist velocity.
2. Measured mean wrist velocity and acceleration rates were high in all planes of motion during pliers tying.
3. Tying rebar using the BPT significantly reduced hand and wrist movements that can cause upper limb WMSDs. Deep forward bending was still necessary to tie the rebar, but the 'free' arm supported the weight of the trunk, reducing forces on the L5/S1 disc.
4. Tying rebar using the BPT+E eliminated the sustained deep forward bending required when tying with the pliers and BPT. Wrist movement was significantly lower in all three planes of motion using the BPT+E. Some participants, however, reported hand-wrist effort similar to using the pliers, resulting in a mean hand-activity level score slightly higher than the ACGIH HAL TLV™.
5. Worker productivity increased when the BPT or BPT+E were used during the study.

Recommendations

1. Provide battery powered rebar tiers with extension handles whenever reinforcing ironworkers tie rebar placed at ground level, i.e., bridge and freeway deck, concrete slab, etc.
2. Provide training to workers who will use the extension handle so that they will be able to correctly adjust the height of the handle and limit the distance they extend the BPT+E during tying.
3. Encourage reinforcing ironworkers to use the extension for the battery powered tier when they tie rebar at ground level.
4. Provide ironworkers information to enable them to identify the early signs and symptoms of low back and upper extremity musculoskeletal disorders.
5. Future research should be conducted to characterize the following aspects of tying reinforcing steel:
 - (a) the types of reinforced concrete construction that would benefit from the use of power tiers;
 - (b) the optimal design of an extension handle for power rebar tiers; and
 - (c) reinforcing ironworkers biomechanical loading, especially to the back and shoulders, during rebar manual material handling.

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Figure 1

MAX-USA RB-392 Power rebar tier (BPT)

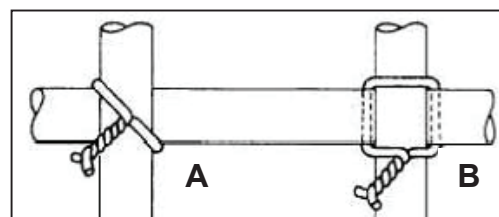


RB-392 Specifications

Max Wraps per Tie	3
Tying Speed	1
Second Max Rebar Size (in)	3/4 to 1-1/2
Wire Gauge	21
Ties per Coil of Wire	180 – 210
Ties per Battery Charge	8000
Voltage	9.6 DC
Weight	4.6 lbs.

Figure 2

Ties used to secure rebar together



A Snap or simple tie (similar to tie made using power rebar tier, except the powertier wraps wire around bars 3 times)

B Saddle tie

Figure 3
Rebar tying using pliers and tie-wire



Pliers

Figure 4

Rebar tying using MAX-USA RB392 battery powered rebar tier



Battery
powered tier

Figure 5

MAX-USA RB-392 Battery powered tier with adjustable extension (BPT+ E)
(plan to use image from manufacturer)



**Adjustable
extension**

Figure 6

Rebar tying using MAX-USA RB392 power rebar tier with adjustable extension handle

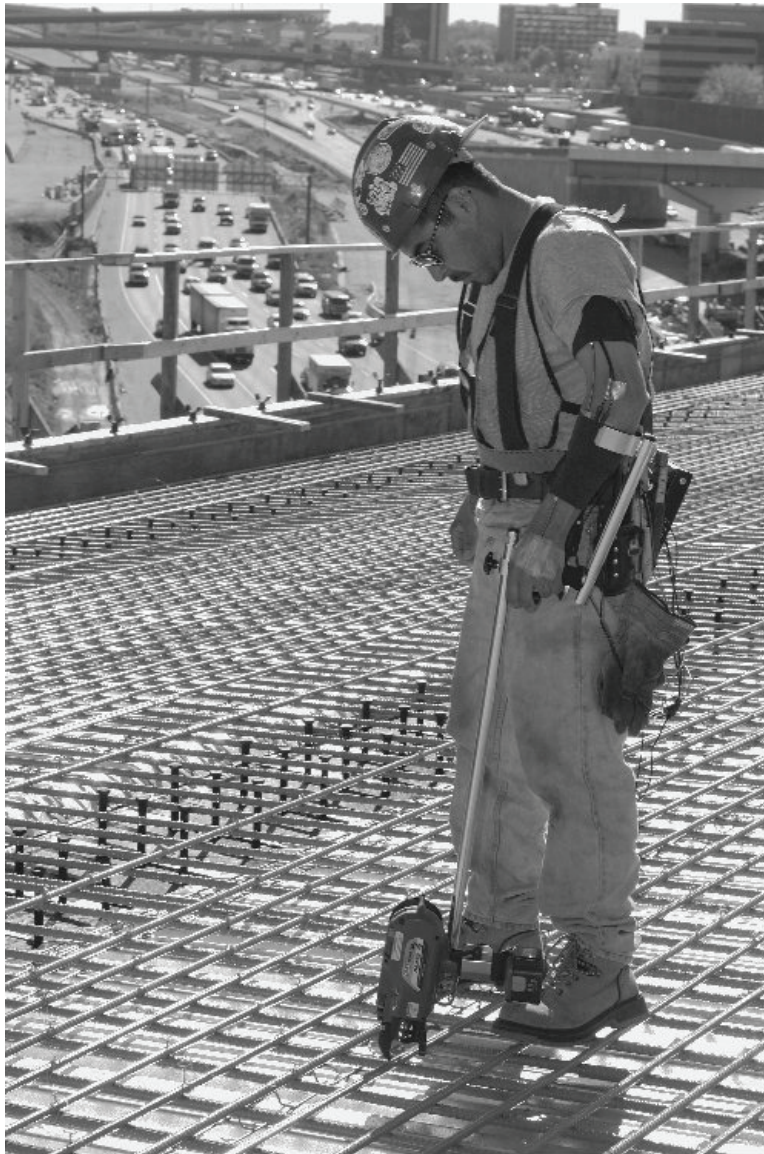


Figure 7

Wrist, hand and arm position/movement planes

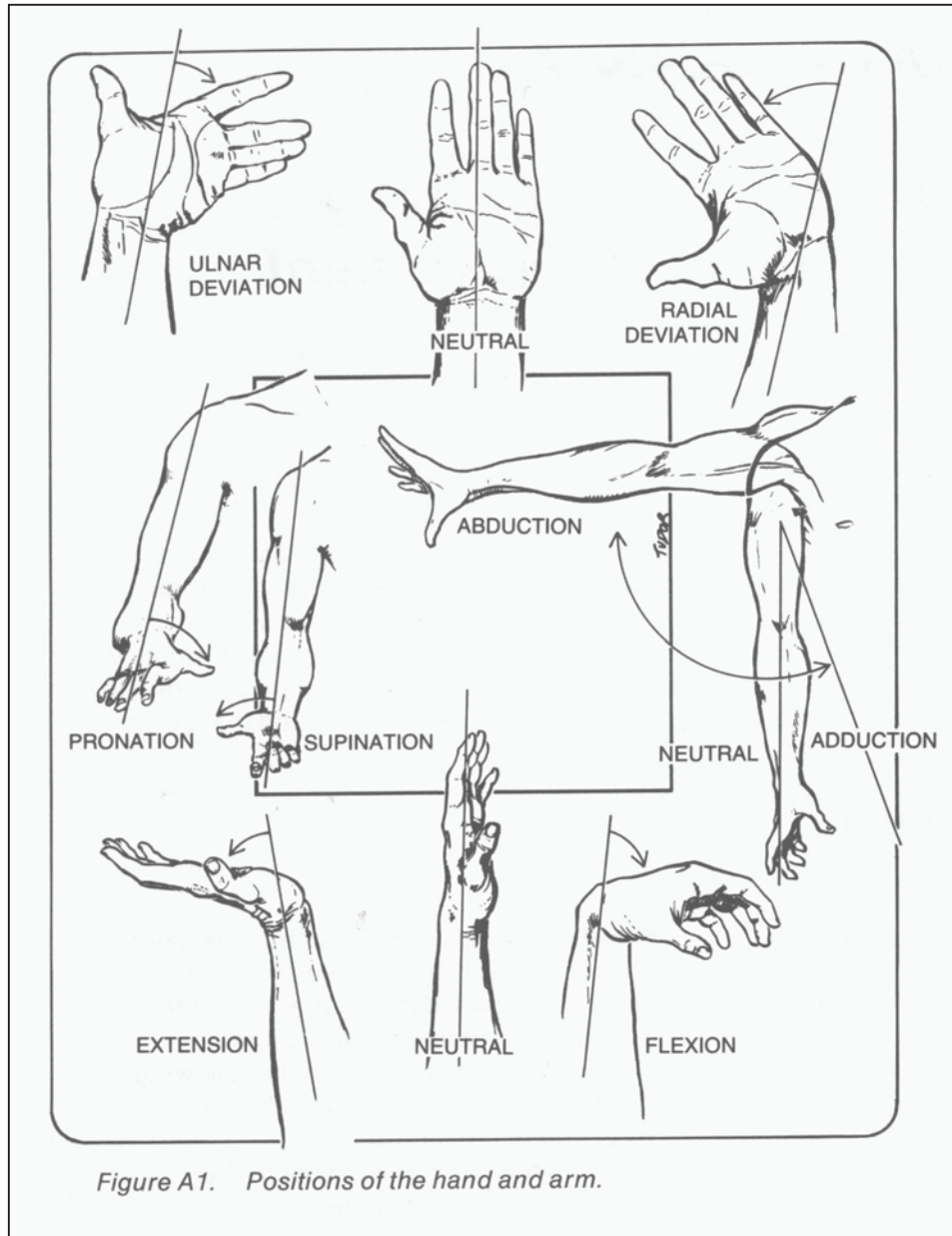
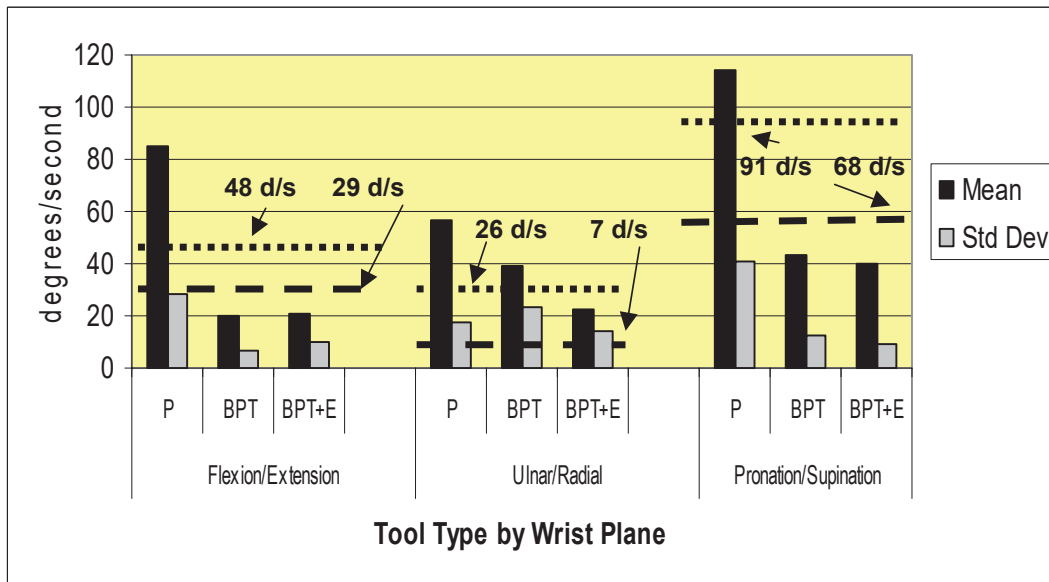


Figure A1. Positions of the hand and arm.

Figure 8
Measured Wrist Velocity during Rebar Tying

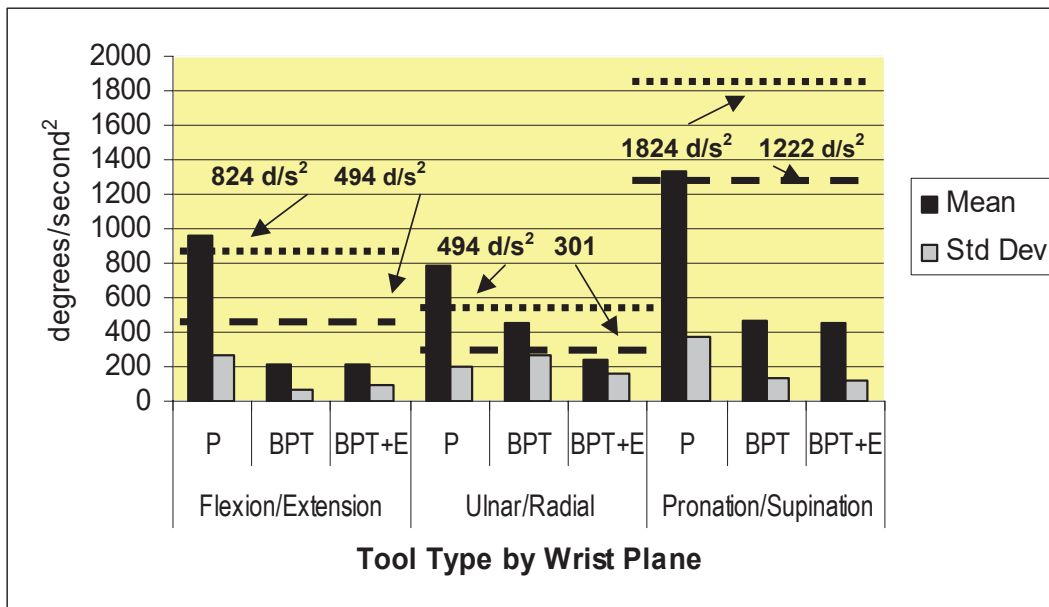


Mean High CTD Risk Mean Low CTD Risk - - - - -

P= Pliers; BPT= Battery powered tier; BPT+E= BPT + extension

Wrist acceleration mean and standard deviations measured in three planes (flexion/extension, ulnar/radial & pronation/supination) during rebar tying and mean high and low CTD risk acceleration rates.⁷

Figure 9
Measured Wrist Acceleration during Rebar Tying



Mean High CTD Risk Mean Low CTD Risk - - - - -

P= Pliers; BPT= Battery powered tier; BPT+E= BPT + extension

Wrist acceleration mean and standard deviations measured in three planes (flexion/extension, ulnar/radial & pronation/supination) during rebar tying and mean high and low CTD risk acceleration rates.⁷

Figure 10

Calculation of one-year cumulative load on L5/S1¹²:

Assumptions: Rodman works 180 days per year tying rebar with pliers an average 4 hours per day and carries materials, i.e., rebar, weighing 20 kg an average 1 hour per day. Extreme forward bending involved in tying rebar at – (a), -105° (b) and -115° (c) 90°. (Table 16) Force on lumbar spine from carrying 20 kg load in front or beside the body equals 2700 N (Seidler et al, 2001).

$$\text{DAYS} \sqrt{8h * \sum_i F_i * t_i} \quad \text{Days} = \text{working days/year}; t_i = \text{average daily duration of activity}$$

(h)

(a)

$$1 \text{ yr} = 180 \sqrt{8h * (1721^2 N^2 * 4h) + (2700^2 N^2 * 1)} = 1.8 \times 10^7 \text{ N-hr}$$

$$5 \text{ yr} = 9.1 \times 10^7 \text{ N-hr}$$

$$10 \text{ yr} = 18.2 \times 10^7 \text{ N-hr}$$

(b)

$$1 \text{ yr} = 180 \sqrt{8h * (2093^2 N^2 * 4h) + (2700^2 N^2 * 1h)} = 2.2 \times 10^7 \text{ N-hr}$$

$$5 \text{ yr} = 10.9 \times 10^7 \text{ N-hr}$$

$$10 \text{ yr} = 21.8 \times 10^7 \text{ N-hr}$$

(c)

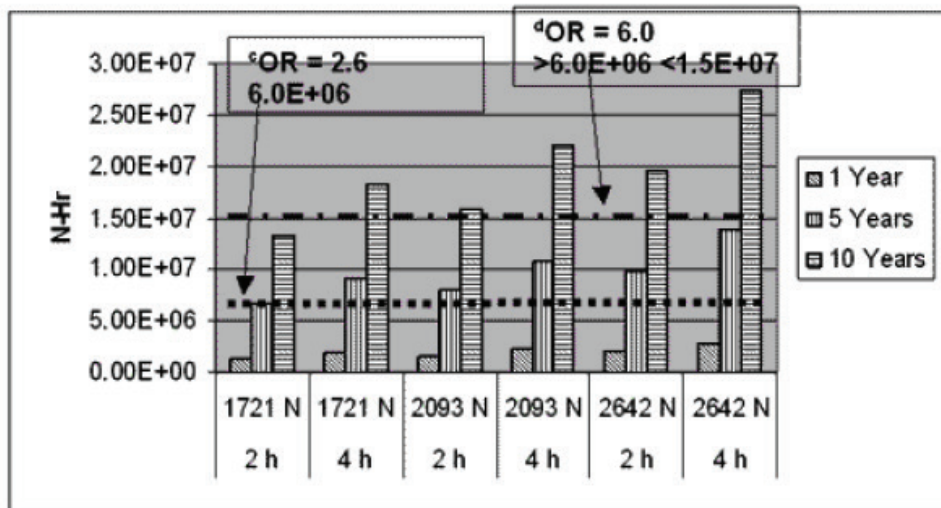
$$1 \text{ yr} = 180 \sqrt{8h * (2642^2 N^2 * 4h) + (2700^2 N^2 * 1h)} = 2.7 \times 10^7 \text{ N-hr}$$

$$5 \text{ yr} = 13.7 \times 10^7 \text{ N-hr}$$

$$10 \text{ yr} = 27.3 \times 10^7 \text{ N-hr}$$

Figure 11

Estimated Cumulative L5/S1 Spinal Disc Loading During Rebar Tying and Carryingband Risk of Developing Spinal Disease with Chronic Complaints¹²



^a See equation in Figure 10.12

^b See Table 19 for estimated spinal loading during tying and carrying.

^c Risk of developing lumbar spondylosis with chronic complaints with or without disc herniation Odds Ratio (OR) = 2.6 (95% CI 1.2-5.7).

^d Risk of developing lumbar spondylosis with chronic complaints with or without disc herniation Odds Ratio (OR) = 6.0 (95% CI 2.7-13.4).

Table 1
Anthropometrics of Subjects

Age	Ht (in.)	Wt. (lb.)	BMI ¹	
42	71	185	25.8	
33	66	160	25.8	
44	71	210	29.3	
40	70	210	29.3	
37	67	160	25.1	
29	68	190	28.9	
30	70	185	26.5	
43	65	170	28.3	
Mean (SD)	37 (6)	69 (2.2)	184 (18.5)	27.4 (1.6)

¹ Body mass index (BMI) calculated using CDC BMI calculator.

Table 2
Ironworker Work History (months)

	Mean	SD	Min	Max
Time tying rebar	124	96.4	29	298
Time with current employer	38	37.7	18	136
Time on current job site	16	12.6	0	32

Table 3
Comparison of Mean Wrist Velocity Postures by Rebar Tying Method
(Chi Square Difference of Least Squares Means)

Plane	Pliers vs. BPT ¹	Pliers vs. BPT+E ²	BPT vs. BPT+E
Flexion/Extension	<0.0001	<0.0001	NS
Ulnar/Radial	NS	<0.05	NS
Supination/Pronation	<0.0001	<0.0001	NS

¹ BPT = MAX RB 392 power tier

² BPT+E = MAX RB 392 power tier plus adjustable extension

³ NS = Not significant.

Table 4

Comparison of Mean Wrist Acceleration by Rebar Tying Method
(Chi Square Difference of Least Squares Means)

Plane	Pliers vs. BPT ¹	Pliers vs. BPT+E ²	BPT vs. BPT + E
Flexion/Extension	<0.001	0.001	NS
Ulnar/Radial	<0.05	0.0009	NS
Supination/Pronation	<0.0001	<0.0001	NS

¹BPT = MAX RB 392 power tier

²BPT+E = MAX RB 392 power tier plus adjustable extension

³NS = Not significant.

Table 5

Participant (n=5) Self Reported Ratings of Perceived Effort¹ during Rebar Tying

Perceived Effort	Pliers	Power Tier	Power Tier + Extension
Hand-Wrist	5.2	2.8	5.0
Low Back	5.8	2.8	1.2

¹Borg 10 Point Perceived effort scale²

Table 6

ACGIH Hand-Activity Level (HAL)⁶ Scores^a for Mean Hand-Wrist
Effort Tying Rebar Using Pliers, BPT & BPT + E

Effort ^b	Pliers	BPT	BPT + E
Mean	2.5 ^c	0.5 ^d	0.8 ^c
Low	1.0 ^c	0.3 ^d	0.3 ^d
High	3.5 ^c	1.0 ^c	1.2 ^c

^aScores <0.56 are acceptable; scores ≥0.56 and ≤0.77 are at the action level; and scores ≥0.78 exceed the TLV.

^b participants' (n=5) response (mean, low & high) on Borg 10 point perceived effort questionnaire.

^c ≥ TLV.

^d<TLV.

Table 7
Time (seconds)^a in Trunk Postures during Rebar Tying

Treatment	Posture	Mean(sec)	%Time	SD	Min	Max
BPT + E	Neutral	124 ^b	83	35	55	150
	16-30	24 ^c	16	36	0	95
	31-45	1	<1	3	0	8
	46-60	<1	<1	<1	0	1
	61-75	<1	<1	<1	0	<1
	76-90	0	0	0	0	0
	>90	0	0	0	0	0
	BPT	Neutral	<1	<1	1	0
16-30		<1	<1	<1	0	<1
31-45		<1	<1	<1	0	<1
46-60		<1	<1	<1	0	<1
61-75		<1	<1	<1	0	1
76-90		5 ^c	3	7	0	18
>90		140 ^b	93	13	110	150
Pliers		Neutral	0	0	0	0
	16-30	0	0	0	0	0
	31-45	0	0	0	0	0
	46-60	<1	<1	<1	<1	1
	61-75	<1	<1	1	0	2
	76-90	6 ^c	4	7	1	23
	>90	141 ^b	93	9	126	150

^aTotal sample time = 150 seconds

^b p < 0.0001 (Comparing differences between BPT + BPT+E and pliers + BPT+E)

^c p < 0.05 (Comparing differences between BPT + BPT+E and pliers + BPT+E)

Table 8
Percent Time Free Arm Used to Supported Trunk during Extreme Flexion
Using Power Rebar Tier per Participant

	P1	P2	P3	P4	P5	P6	P7	P8
Supported ^a	94.9%	91.0%	92.3%	89.5%	86.4%	98.3%	96.6%	90.0%
Unsupported	5.1%	9.0%	7.7%	10.5%	13.6%	1.7%	3.4%	10.0%

^aIronworkers used the free hand or forearm to support an unknown proportion of their head/trunk weight

Table 9
Estimated Forces on the L5/S1 Disc Using the 3D SSPP4







	Trunk	Angle	Total Compression	Total Shear
	Flexion Rotation Lateral	-90° 0° 0°	2427 N	389 N
	Flexion Rotation Lateral	-90° 0° +/- 25°	2857 N	306 N
	Flexion Rotation Lateral	-105° 0° 0°	1864 N	419 N
	Flexion Rotation Lateral	-105° 0° +/- 25°	2322 N	480 N
	Flexion Rotation Lateral	-115° 0° 0°	1511 N	401 N
	Flexion Rotation Lateral	-115° 0° +/- 25°	1930 N	501 N

Table 10

Estimated Cumulative Physical Workload (N-hb) on the Low Back (L5/S1)
Due to Extreme Forward Flexion after 1, 5, and 10 Years

Flexion	Newtons	Hrs/Day	Days/Wk	Wk/Yr	N-h/1 Yr	N-h/5 Yr	N-h/10 Yr
90 deg	2642	2	5	36	0.9E+06	4.8E+06	9.5E+06
		4	5	36	1.9E+06	9.5E+06	19.0E+06
		6	5	36	2.9E+06	14.0E+06	29.0E+06
105 deg	2093	2	5	36	0.7E+06	3.8E+06	7.5E+06
		4	5	36	1.5E+06	7.5E+06	15.0E+06
		6	5	36	2.3E+06	11.0E+06	23.0E+06
115 deg	1721	2	5	36	0.6E+06	3.1E+06	6.2E+06
		4	5	36	1.2E+06	6.2E+06	12.0E+06
		6	5	36	1.9E+06	9.3E+06	19.0E+06

^a Equation used to calculate annual load on L5/S1 shown in Figure 6¹²

^b N-h=Newton-hours

Table 11

Number of Ties Completed in 2.5 Minutes by Treatment

Subject	Pliers	BPT	BTP+E
1	47	85	55
2	31	71	41
3	44	89	54
4	48	99	58
5	36 ^a	69	53
6	51	93	66
7	37	79 ^b	38
Mean	42	84	52
SD	6.8	10.3	9.0

^a Adjusted for 2'15" sample period.

^b Adjusted for 2'23" sample period.



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